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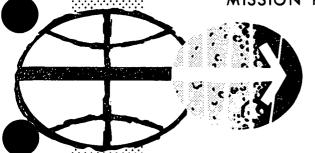
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NASA/DOD EARTH ORBIT
SHUTTLE TRAFFIC MODELS
BASED ON SIDE-BY-SIDE

LOADING OF PAYLOADS

Flight Analysis Branch

MISSION PLANNING AND ANALYSIS DIVISION



MANNED SPACECRAFT CENTER HOUSTON.TEXAS

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NASA/DOD EARTH ORBIT SHUTTLE TRAFFIC MODELS BASED ON SIDE-BY-SIDE LOADING OF PAYLOADS

By R. E. Kincade, M. E. Donahoo, and W. R. Pruett Flight Analysis Branch

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MISSION PLANNING AND ANALYSIS DIVISION NATIONAL AERONAUTICS AND SPACE ADMINISTRATION MANNED SPACECRAFT CENTER HOUSTON, TEXAS

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CONTENTS

Section		Page
1.0	SUMMARY	1
2.0	INTRODUCTION	2
3.0	SYMBOLS AND ABBREVIATIONS	2
4.0	GROUND RULES	3
5.0	DISCUSSION	3
6.0	COMMENTS	7
	REFERENCES	80

TABLES

ľable		Page
I	OSSA PRIORITY ASSIGNMENT	9,
II	MAXIMUM NUMBER OF EOS FLIGHTS WHICH CAN BE FLOWN FOR THE PERIOD 1978 THROUGH 1981	10
III	NASA AND NON-NASA (EXCLUDING DOD) PAYLOAD CHARACTERISTICS AND FREQUENCIES	11
IA	CHARACTERISTICS OF THE REUSABLE TUG, CENTAUR, AGENA, AND FW-4S	17
v :	EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979	
	(a) 1979 (b) 1980 (c) 1981 (d) 1982 (e) 1983 (f) 1984 (g) 1985 (h) 1986 (i) 1987 (j) 1988 (k) 1989 (l) 1990	18 19 21 24 27 30 33 36 39 42 45 48
VI	EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPA-BILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985	
	(a) 1979 (b) 1980 (c) 1981 (d) 1982 (e) 1983 (f) 1984	51 52 54 56 58 60
VII	EOS FLIGHTS ASSOCIATED WITH TWO TUG AVAILABILITY TIMES, 1979 AND 1985	62

Table		Page
VIII	NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS BY INCLINATION	
	(a) Tug available in 1979 and payloads stacked side-by-side	63
	stacked side-by-side	03
	loaded side-by-side	65
IX	TOTAL PAYLOAD TO ORBIT (LB)	
	(a) Tug available in 1979 and payloads	
	loaded side-by-side	67
	(b) Tug available in 1985 and payloads	(0
	loaded side-by-side	69
X .	ENERGY STAGES REQUIRED	
	(a) Tug available in 1979 and payloads	
•	loaded side-by-side	71
	(b) Tug available in 1985 and payloads loaded side-by-side	70
	loaded Side-by-side	72
XI	NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS PER YEAR	73
XII·	NUMBER OF FLIGHTS REQUIRING OFFLOADING OF OMS OR REMOVAL OF ABES	
	(a) Tug available in 1979 and payloads	
	loaded side-by-side	74
	(b) Tug available in 1985 and payloads	
	loaded side-by-side	76

NASA/DOD EARTH ORBIT SHUTTLE TRAFFIC MODELS

BASED ON SIDE-BY-SIDE LOADING OF PAYLOADS

By Richard Kincade, Michael Donahoo, and William Pruett

1.0 SUMMARY

This report is the second of two documents written to present optimized Earth Orbit Shuttle traffic models for the years 1979 through 1990 and will partially fulfill the requirements of reference 1 for NASA/DOD traffic model and fleet sizing analyses. The first report, reference 2, defines two traffic models—one based on a tug availability date of 1979 and the other on a tug availability date of 1985—assuming only end-to-end loading of payloads on the tug are possible. This second study is conducted under the same groundrules as those employed for the analysis of reference 2 with one exception; the satellites are allowed to be stacked side-by-side on the tug.

Reference 2 analyzes end-to-end placements of the satellites on the tug since other studies had indicated that phasing maneuvers between deployments of the satellites are apt to present more problems for side-by-side stacking than for end-to-end loading. Unknowns associated with tug c.g. limits, gimbal limits for alining the thrust through the c.g., and structural loadings resulting from side-by-side stacking of cargo dictated that end-to-end loadings be evaluated first. Side-by-side placements are considered in this study to provide the reader with the information necessary to determine EOS flight savings from those of reference 2 which could be realized if side-by-side loadings were possible.

As stated in reference 2, it is not intended to advocate one type loading over another; rather, it is an attempt to identify the number of EOS flights for each. There should be sufficient information in the two documents for mission planners and decision makers to make realistic and reasonable judgements on which loading method should be used for the EOS program.

2.0 INTRODUCTION

To obtain the most economical usage of the EOS, it is imperative that the maximum number of missions should be accomplished with the minimum number of EOS flights. A number of traffic model and fleet sizing studies are anticipated prior to actual mission planning for the EOS program. The purpose of this report is to present optimized EOS traffic models associated with two possible reusable tug availability dates and side-by-side loading of satellites on the tug or booster using the NASA and DOD payload information obtained from OSSA, Space Station, and DOD mission models generated specifically for this purpose.

At the time this traffic model was being defined the DOD was updating their mission models; therefore, this report does not reflect the official DOD program. However, DOD missions used in this report and contained in reference 3 are considered to be representative.

3.0 SYMBOLS AND ABBREVIATIONS

ABES	Air Breathing Engine Subsystem
DOD	Department of Defense
EOS	Earth Orbit Shuttle
fps	feet per second
h _a	height of apogee
h _p	height of perigee
NASA	National Aeronautics and Space Administration
n. mi.	nautical mile
OMS	Orbital Maneuvering System
OSSA	Office of Space Science and Applications
ΔV	change in velocity

4.0 GROUND RULES

The missions of the traffic models were combined into EOS payloads according to the groundrules defined in reference 1 and listed below:

- a. NASA and DOD missions shall be flown separately.
- b. The maximum number of payloads carried on a single mission should not exceed three.
- c. The payloads should be integrated into the EOS cargo compartment either end-to-end or side-by-side. Payloads should not be stacked atop each other.
- d. Each mission needing an energy stage for payload placement requires a dedicated EOS flight.
- e. The EOS capability to be used is presented in figure 1. The preferred mode of operations is with ABES on and OMS propellant equivalent to 1500 fps in the tanks. Those missions on which OMS or ABES must be offloaded to gain necessary capability should be identified.
- f. The first 10 EOS flights are not to be analyzed. These flights will be identified in detail by the NASA Headquarters.
- g. Starting with NASA flight number 5 and DOD flight number 3 in 1979, the choice of payloads is to be based on the NASA priorities defined in table I. The DOD missions are to be selected from reference 3, with the mission at the bottom of the table having the highest priority and the mission at the top of the page (first of the alphabet) having the lowest priority.
- h. It should be assumed that the EOS has the capability to fly all payloads starting in 1982.

5.0 DISCUSSION

The EOS, as it is presently designed, has the capability (figure 1 defines payload weight as a function of inclination) to accomplish, without the assistance of a boost stage, a little more than half of the NASA flights planned for the period from 1978 through 1990 with these flights encompassing Space Station, sortie, automated spacecraft, man-tended spacecraft and non-NASA (excluding DOD) missions. Based on the DOD information supplied for this study, approximately 40 percent of the DOD flights are assumed to require booster or tug assistance.

In previous traffic models, kick stages such as the Centaur, Agena and FW-4S or a reusable tug have been used for satellite placement when the EOS did not have the capability. These studies have assumed that the tug could take 10 000 pounds to an equatorial geosynchronous orbit from the basic EOS 100 n. mi. circular orbit inclined 28.5° and then return empty to the EOS. The request made in reference 1 specifies that all traffic models shall be designed using a tug with half this capability (the capability curves for this tug are presented in figure 2) and that boosters shall be employed for those years in which the tug is not available.

Another difference between the traffic models of this report and others derived in the past will be found in the methods used in determining the total payload weights. Other traffic models assumed the tug carried a full load of fuel for every mission in order to insure that there would be enough propellant for any required phasing and rendezvous maneuver. Minimum fuel usage computations assume that transfers from one **orbit** to another are the only maneuvers that are required.

Although neither maximum nor minimum fuel consumption present a truly accurate account of the number of EOS flights required, minimum fuel loading would be more nearly correct because it is not envisioned that large amounts of propellant will be needed for phasing and terminal rendezvous maneuvers. Therefore, minimum fuel usage is assumed in this study for all tug flights.

The above tug data plus the groundrules presented in section 4.0 constitute the basis for the two traffic model studies described in this report. For both models, every attempt is made to combine payloads with similar inclination and destination characteristics. Lengths, diameters and weights of the cargo are also prime factors in the combination process (the cargo bay dimensions are 15 X 60 feet while the maximum payload which can be carried to the low earth parking orbit varies according to the inclination of the orbit). Combination of two identical satellites is not done unless specifically called for in the mission models of reference 1 or, if necessary, to keep the EOS flights at a minimum. At no time is a combination of a NASA and DOD payload allowed. Very little is known about either NASA or DOD packaging and mounting factors; and therefore, these items are not considered in the side-by-side stacking combinations. In the years when the tug is available, booster stages are used only when the tug does not have the capability to place the payload in orbit.

The number of EOS flights, both NASA and DOD, planned for the years 1978 through 1981 (table II) limits the number of missions which can be performed by the EOS during this period. The first 10 flights, 4 in 1978 and 6 in 1979, are to be defined in detail by NASA Headquarters

and are not included in the traffic models but are shown in some of the tables presenting total EOS flights.

Because the number of EOS flights required for the 1978 through 1981 period greatly exceeds the maximum number of flights planned, the OSSA priorities listed in table I are used as the basis for NASA payload selection. The highest priority for DOD missions starts at the bottom of the DOD payload characteristics and frequencies table of reference 3 and works up the table with the mission listed at the top having the lowest priority. If all DOD missions could not be accommodated on the limited number of flights, an attempt is made to include at least one of each type.

After the year 1981, no restrictions are placed on the number of EOS flights, thus an unlimited traffic model exists for the period from 1981 through 1990. The frequencies and payload characteristics of the NASA mission model are presented in table III while reference 3 contains the frequencies and payload characteristics for DOD missions.

The amount of propellant used determines the tug life. In this study, the tug is considered to be expended after 500 000 pounds of propellant have been consumed by the tug engines. As mentioned previously, minimum tug fuel consumption is assumed for each flight of these traffic models. Actual fuel usage considering all station-keeping, phasing, transfer and other rendezvous and docking maneuvers will increase the fuel usage but is impossible to calculate at the present time since the missions are so ill defined. The addition of the tug fuel necessary to perform these maneuvers should not increase the number of tugs expended significantly. The boosters are flown with the fuel tanks full in order to keep computation time to a minimum.

For sun synchronous payload placements by the tug, the EOS is placed in a 90° inclination orbit and the tug makes the plane changes. In this way the OMS propellant offloaded is less than tug propellant consumed, thus increasing the efficiency of the EOS. The EOS makes the plane changes for FW-4S payload placement because the FW-4S is so light.

The characteristics of the reusable tug along with those for the various non-reusable booster stages are presented in table IV. The tug data was extracted from reference 1 while booster information was obtained from reference 4. Figure 2 defines the tug capability as a function of ΔV .

The actual combination of payloads, both NASA and DOD, for side-by-side loadings are defined in tables V and VI for the tug availability dates of 1979 and 1985, respectively. The payload designation definition for the NASA missions of table V can be found in table III. The definition of DOD mission designations are contained in reference 3. It should be

noted that the EOS flights of tables V and VI would not necessarily be flown in the order presented. Expediency in selecting the payloads and simplicity of the methods used in the analysis dictated the order in which the flights are presented in these tables.

Tables V and VI are further reduced to the number of EOS flights and the total number of payloads associated with these flights (table VII). The number of EOS flights by inclination (table VIII), the total payload taken to orbit (table IX), the energy stages required (table X), and the number of EOS flights per year (table XI) are tabulated for information.

The traffic models indicate that when the tug will be in service starting in 1979, 827 missions are accomplished on 615 EOS flights. As a comparison, 670 flights (452 NASA and 218 DOD) are needed for 811 missions (564 NASA and 247 DOD) when only end-to-end loading of the payload is allowed. Of the 615 flights, 419 carry NASA payloads--574 missions--while 196 carry DOD payloads--253 missions. Combinations of NASA and DOD payloads are not permitted and, therefore, are not attempted. One hundred and sixty of the 419 NASA flights and 73 of the 196 DOD flights require tugs.

The traffic model for the second tug availability date of 1985 consists of 594 EOS flights (833 missions) and these flights are relegated to 399 flights for the 580 NASA missions and 195 flights for the 253 DOD missions. Reference 2 shows that 642 flights, 430 NASA and 212 DOD, are required to carry a total of 832 missions--578 NASA and 254 DOD--for end-to-end loadings. Tugs are used on 86 of the NASA flights and 40 of the DOD flights when payloads are stacked side-by-side. The first 10 EOS flights are not included in any of the above numbers.

The first traffic model requires the expenditure of 14 tugs for NASA missions (table X). Thirteen of these 14 are expended because the tug does not have the ΔV capability to return to the EOS after satellite placement. However, this is not as big a waste of tugs as it might first appear because if the tugs that are expended in the traffic model could return to the EOS, 10 tugs would still have to be retired based on 500 000 pounds of fuel consumption constituting the retirement of a tug. DOD missions result in the expenditure of seven tugs, all resulting from 500 000 pound propellant usage. Totalling the two organizations tug expenditures together, 21 tugs are expended.

When the tug is not used until 1985, 14 tugs are required to be expended with NASA and DOD missions accounting for 10 and four tugs, respectively. All 10 of the tugs expended for the NASA flights are attributed to the tug not having the capability for a round trip (six tugs would be retired by the fuel usage requirement even if all 10 of the tugs could be returned). All DOD tug expenditures result from normal tug retirement.

In the event the weight of the tug plus satellites exceeds the nominal designed payload capabilities of the EOS, either OMS propellant is offloaded or the ABES is removed in order to gain the necessary capabilities. In this study, it is assumed that OMS propellant offloading (maximum allowed to be offloaded is equivalent to a ΔV of 600 fps at an inclination of 28.5° and 500 fps at an inclination of 90°) will be considered first, and the ABES will be removed only if the EOS still cannot perform orbit insertion after OMS propellant reduction.

For the first traffic model, 133 flights (106 NASA and 27 DOD) require offloading of OMS and 15 flights (12 NASA and three DOD) cannot be performed without the removal of the ABES. If the tug does not become available until 1985, the total number of flights requiring either offloading of OMS or removal of ABES drops to 84 and 10, respectively. No NASA flights require both the removal of the ABES and the offloading of OMS. One DOD flight in the first traffic model requires both the removal of the ABES and the offloading of OMS. Table XIII further identifies those flights requiring the removal of the ABES or offloading of OMS propellant.

6.0 COMMENTS

When the tug is available in 1979, approximately 29 percent of the EOS flights carrying NASA cargo require either offloading of OMS propellant or the removal of the ABES to accomplish the flight. The percentage for DOD flights is approximately 17 percent. For the 1985 availability date, the percentages drop to roughly 21 percent and 6 percent for NASA and DOD, respectively. The reason for these offloadings is that large amounts of tug propellant are necessary to place the satellites in orbit. This is especially true for equatorial geosynchronous orbits where 40 000 to 49 000 pounds of propellant are required for a round trip and the maximum weight the EOS can take to the 100 n. mi. circular orbit at a 28.5° inclination without OMS fuel reduction or ABES removal is 50 000 pounds. Although not nearly as much propellant is required for a polar or sun synchronous orbit, the situation is just as bad for these high inclination orbits since the inert weight of the tug is approximately one half of the payload capability of the EOS with the ABES on and full OMS AV fuel loading.

There is probably no way the tug characteristics can be changed such that less fuel is needed for the equatorial geosynchronous orbits. However, it does seem feasible to use some small solid stages such as the FW-4S for satellite placements in polar and sun synchronous orbits since it was found that the size of the tug was the reason that two EOS flights were often needed to complete these missions. The use of these small solid stages should save approximately 10 flights over the 12-year period

and would eliminate the necessity for offloading of OMS propellant or the removal of the ABES for the polar and sun synchronous orbit missions.

In conclusion, this analysis has attempted to take the groundrules of reference 1 and define the most optimum traffic models for the two tug availability dates and side-by-side stacking of the NASA and DOD payloads. A similar report concerned with end-to-end loadings is contained in reference 2 for comparison purposes. No recommendations are made as to which method of payload integration on the tug should be planned for in the future. The decision on which mode of cargo loading will be used is left to NASA management.

TABLE I. - OSSA PRIORITY ASSIGNMENT

	Total	6		16		1,1		9	5	45	122
ij	81								1	81.	19
Priority III	80-	·								12	12
Pric	79								3.	15	18
II	81			; ·		5 4 7					16
Priority	80					# m 9			τ		1,1
Pr	79					6 1 5					टा
I	81	6		400				1 2			20
Priority I	80			9				2			8
Pri	79			2		•		Н			۳
	Mission	Space station	Sortie	Type 1 Type 2 Pallet	Automated S/C	Comm/nav Earth obs. Physics/astr.	Man tended	LST HEAO revis.	Planetary	Non-NASA	TOTAL

TABLE II.- MAXIMUM NUMBER OF EOS FLIGHTS WHICH

CAN BE FLOWN FOR THE PERIOD 1978-81

	^a 1978	^b 1979	1980	1981
NASA .	3	10	24	34
· DOD	1	Ъ	12	16

^aThe flights for the year 1978 will be defined by NASA headquarters.

bFour of the NASA flights and two of the DOD flights will be defined by NASA headquarters for the year 1979.

TABLE III.- NASA AND NON-NASA (EXCLUDING DOD) PAYLOAD CHARACTERISTICS AND FREQUENCIES

(a) Physics and astronomy

Payload		F	Payload character	ristics	F	inal orbital paramet	ers							Year					·	
designation	Satellite name	Diam . ft.	Lgth. ft.	Wt. lb.	i	h _a	hp	78	79	80	81	82	83	84	85	86	87	88	89	90
1	Astronomy explorer	2	3	720	28.5	270	270	1	2		1	2	2	1		2	1	2	2	
2	Radio explorer	5	4	720	28.5	19 300	19 300	1		2	1		İ	1	1 2	_	$\bar{1}$	_	_	2
! 3	Low magnetosphere explorer	4	8	1 200	0-90	1 800	180	1 (90)	1 (0)	1(28.5)	1(55)	1(90)	1(0)	1(28.5)	1(55)	1(90)	1(0)	1(28.5)	1(55)	1(90)
4	Middle magnetosphere explorer	6	8	1 000	0-90	20 000	1 000	1 (90)	1 (0)	1(28.5)	1(55)	1(90)	1(0)	1(28.5)	1(55)	1(90)	1(0)	1(28.5)	1(55)	1(90)
5	High magnetosphere explorer	4	6	600	0-90	1.0 A.U:	Any	1 (90)	1 (0)	1(28.5)	1(55)	1(90)	1(0)	1(28.5)	1(5 5)	1(90)	1(0)	1(28.5)	1(55)	1(90)
6	Orbiting solar observatory	7	10	1 900	28.5	350	350	1		l ı	1				}					
7	Gravity/relativity experiment (C, E)	5	7	1 500	90	300	300			1				1 ^C						1 ^E
8	Gravity/relativity experiment (B. D)	4	5	500	28.5	1.0 A.U.	1.0 A.U.				1 ^B			•			10			
9	Radio interferometer	12	15	6 000	28.5	38 300	38 300				1									ļ
10	Solar orbit pair synchronous	10	12	1 900	30	19 300	19 300			1				,	į	İ			,]
11	Solar orbit pair 1 A.U.	10	12	1 900	28.5	1.0 A.U.	1.0 A.U.	1]		<u> </u>	1 1		1			†	1
12	Optical interferometer pair	7 ea	10 ea	3 500 ea	30	19 300	19 300	l		1				1				2	1	ì
13	High energy stellar astronomy observatory (HESA®)	14	46	21 000	30	230	230	ļ	1 (up)			1(up)	l(down)		1(up)		1 (down)	-	1 (up)	
14	HESA@ revisit	14	13	3 500	30	230	230	1) 2)	2) 2	2	2	2	2)	2	2
15	Large space telescope (LST-RAM)	14	60	30 000	28.5	350	350				I(up)	-	_	_	1(down) 1(up)		_		-	
16	LST-RAM revisit	14	13	3 500	30	350	350					2	2	2	1 1	, ,	2	,	,	1 2
17	Large solar observatory (LSO)	14	54	27 000	30	350 350	350	1		ł		} ~	1(up)	_	1 *	1	1	1(d), 1(u)	2	1 2
18	LSO revisits	14	13	3 500	30	350	350			1	1	1		2	2	2	1 2	1 1 1	2	2
19	Large radio observatory (LRO)	14	30	19 300	30	350	350			1				_	1(up)		-	1	_	
20	LRO revisits	14	13	3 500	30	350	350		-	1	1	ļ			_ '	2	2	2	2	2

(b) Earth observations (R and D)

Payload			Payload characte	ristics	F	inal orbital paramet	ters		/		•			Year		· ·				
designation	Satellite name	Diam. ft.	Lgth. ft.	Wt. lb.	i	h _a	h _p	78	79	80	81	82	83	84	85	86	87	88	89	90
21	Polar earth observation satellite	. 6	12	2 500	99.15	500	500		1	1	1	1	1	1	1	1	1	1	1	1
22	Sync. earth observation sateilite	4	6	1 000	0	19 300	19 300			1		1		1		1		1		1
23	Earth physics satellite	3.5	6.5	600	90	400	400	i		1	1	1	1		1		1		11	
			· · · · · · · · · · · · · · · · · · ·	-					Systems demon	strations		·	·	<u> </u>			,			
24	Sync. meteorological satellite	5	8	1 000	0	19 300	19 300					1	1							
25	Tiros	5	10	1 000	101.1	700	700	İ		l	1]		}	1				ł	1
26	Polar earth resources satellite (take two at a time)	6	12	2 500	99.15	500	500									2	4		·	
. 27	Synchronous earth resources satellite	4	6	1 000	0	19 300	19 300				1	2	1				1	2		

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TABLE III. - NASA AND NON-NASA (EXCLUDING DOD) PAYLOAD CHARACTERISTICS AND FREQUENCIES - Continued

(c) Communications and navigation
(R and D)

Payload		ſ	Payload character	ristics	ı	Final orbital paramet	ers							Year						
designation	Satellite name	Diam. ft.	Lgth. ft.	Wt. Ib.	i	h a	hρ	78	79	80	81	82	83	84	85	86	87	88	89	90
28	Applications technology satellite	15	20	7 950	0	19 300	19 300		1		1		1	1		1		1	1	
29	Small app. technology satellite synchronous	6.5	12	600	0	19 300	19 300	1	1	1	1	1	1	1	1	1	1	1	1	1
30	Small app, technology satellite polar	6.5	12	600	90	3 000	300	1	1	1	1	1	1	. 1	1	1	1	1	1.	1
31	Cooperative application synchronous	6.5	12	820	0	19 300	19 300		1					. 1						
32	Cooperative application polar	6.5	12	820	90	3 000	300					1		 					1	<u></u>
								Sy	stems demonst	ration				1						
33 34 35	Medical network satellite Education broadcast satellite Follow-on system demonstration	12 10 12	15 19 15	2 000 2 145 2 000	0 0 0	19 300 19 300 19 300	19 300 19 300 19 300		2	2	2	2	2	2	2	2	2	2	2	2
									Operationa	ıl				:						
36 37	Tracking and data relay Planetary relay satellite	12 10	15 20	2 300 1 000	0 0	19 300 19 300	19 300 19 300		1 2	2	1		2	1 1	2		2	i	1	2

(d) RAM sortie missions

Do tool		F	Payload character	istics	F	inal orbital paramet	ters							Year				·		· · · · · · · · · · · · · · · · · · ·
Payload designation	Satellite name	Diam. ft.	Lgth. ft.	Wt. Ib.	i	h _a	h _p	78	79	80	81	82 -	83	84	85	86	87	88	89	90
38	General scientific research module sortie	14	54	27 500	55	200	200				2	3	4	4	3	·				
39	General applications module sortie	14	51	30 000	65	100	100				2	3	2	3	2	3		3	1	
40	Dedicated scientific research module-astronomy sortie	14	54	29 500	55	200	200					,		1	3	4	5	4	5	5
41	Dedicated applications module- earth observation sortie	14	41	22 500	75	100	100							, <u> </u>	2	2	2	2	3	4
			,						Pallet-type mo	odule					·					
42	Earth resources sortie	14	37	6 000	90	125	125		_	1	1	2								
43 44	Bio research module sortie Astronomy sortie	14	37 37	4 300 5 700	28.5 28.5	200 200	200 200		1	2	2	2	l ı							ļ
45	Fluid management sortie	14	37	7 100	28.5	200	200			ī	_		l i			ì				
46	Teleoperator sortie	14	37	5 000	28.5	200	200		1	1	_		1	:						į.
47	Manned work platform sortie	14	37	6 700	28.5	200 200	200				1		1	:				[}
48	Large telescope mirror test sortie	14	37	13 000	28.5	200	200		1											
49	Astronomical maneuvering unit sortie	14	37	3 800	28.5	200	200	·		1			<u></u>							

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TABLE III.- NASA AND NON-NASA (EXCLUDING DOD) PAYLOAD CHARACTERISTICS AND FREQUENCIES - CONCLUDED

(e) Planetary

Devland			Payload characteris	stics	F	inal orbital parameters							Year						
Payload designation	Satellite name	Diam. ft.	Lgth. ft.	Wt.	i	ΔV required, fps	78	79	80	81	82	83	84	85	86	87	88	89	90
50	Mars Viking	10	12	7 700	30	15 400		1		1									1
51	Mars sample return	15	22.5	22 000	30	15 400	į					1		1			-	•	. 2
52	Venus explorer	5	12	1 000	30	13 400			1	ĺ					1	1			_
53	Venus radar mapping	10	12	7 900	30	13 400	ŀ				1		}	1				1	İ
54	Venus explorer lander	10	15	7 300	30	13 400	ŀ							1	į	1	1		1
55	Jupiter pioneer orbiter	10	15	900	30	22 700	į				2	İ				1			
56	JUN grand tour	10	12	1 500	30	25 900	1	2	1				1						ł
57	Jupiter tops orbiter/probe	10	15	3 300	30	22 700				ľ			-	1		1		ļ	
58	Uranus tops orbiter/probe	10	15	3 700	30	24 000				ļ			1	1	1			1	
59	Asteroid survey	10	35	27 000	30	13 400	j						1			1			1
60	Comet rendezvous	10	35	24 000	30	13 400				į	1		i	1	1				

(f) Space station

Payload	}	F	Payload characteri	stics		Final orbital paramet	ers							Year						•
designation	Satellite name	Diam. ft.	Lgth. ft.	Wt.	i	h	h _p	78	79	80	81	82	83	84	85	86	87	88	89	90
61	Station module-core (includes refurbishment)	14	′40	20 000	55	270	270				1			1	1	3	2			
62	Station module-others	14	30	20 000	55	270	270				5				3					
63	Crew/cargo	14	30	20 000	55	270	270				l í	6	6	6	6	l 8 l	.8	8	8	8
64	Physics laboratory	14	32	22 000	55	100	270]	i i		1	1	1(up)			1(down)		1(up)		1
65	Cosmic ray laboratory Part I	14	52	30 000	55	270	270					l		Į.				1(up)		į
	Cosmic ray laboratory Part II	14	7	24 000	55	270	270	1	1		1	ł	}			i		1 (up)		ł
66	Life sciences lab	14	58	33 000	55	100	270	İ	1		1(up)	1	1(down)		1(up)	1		- ·		l(down)
67	Earth observation laboratory	14	45	25 000	55	100	270				1(up)		1(down)	 	1(up)					1 (down)
68	Communications/navigation	14	38	19 000	55	100	270				2.00		1(up)		1(down)					l(down) l(up)
69	laboratory Space manufacture laboratory	14	45	25 000	55 ·	100	270													1(up)

(g) Non NASA

			Payload character	istics	Fi	inal orbital paramete	ers						;	Year		· · · · · · · · · · · · · · · · · · ·				
Payload designation	Satellite name	Diam. ft.	Lgth. ft.	Wt.	i	h _a	h _p	78	79	80	81	82	83	84	85	86	87	88	89	90
70 71 72 73 74 75 76	Comsat satellite U. S. domestic communication Foreign domestic communication Navigation and traffic control Navigation and traffic control Tos meteorological Synchronous meteorological	6.5 10 4 5 5 5	12 19 12 8 8 6	1 420 2 145 1 000 700 700 1 000	0 0 0 29 5 101.1	19 300 19 300 19 300 30 000 19 300 700 19 300	19 300 19 300 19 300 16 000 19 300 700 19 300	2 2 2 1 1	2 1 3	1 2 2 1 1 1	1 6 2 1	1 2 1 1	2 2 2 1 1 1	1 2 1 1	1 2 1 1 1	2 4 1 1	2 5 1 1 1	2 2 2 1 1	1 2 1 1 1 1	2 2 1 1
77 78	Polar earth resources (take two at a time) Synchronous earth resources	12 6	15 6	2 500 1 000	99.15 0	500 19 300	500 19 300		4		4		4		4			4		

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TABLE IV. - CHARACTERISTICS OF THE REUSABLE
TUG, CENTAUR, AGENA, AND FW-4S

	Tug	Centaur	Agena	FW-48
Dry weight, 1b	6 818	4 614	1 380	90
Maximum propellant loading, 1b	. 49 550	29 858	13 440	608
I _{sp} , sec	460	442	. 310	283
Dimensions, ft	14.5 × 40	10 × 30	5 × 20	2 × 5

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb	Round trip minimum tug propellant required			
	(a) NASA - 1979						
1	43, 1	14 × 40	5 020	EOS			
. 2	48, 1	14 × 40	13 720	EOS			
. 3	13	14 × 46	21 000	EOS			
14	21, 30	14.5 × 52	^b 22 700	12 800			
5	29, 31	14.5 × 60	^c 49 750	41 500			
· 6	4,5	14.5 × 48	38 700	30 300			

(a) DOD - 1979

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1	None			EOS
2	None		 .	EOS

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100 n. mi. circular orbit.

^COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(b) NASA - 1980

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
ı	42	14 × 37	6 000	EOS
2-3	1 114	14 × 37	5 700	EOS
4	45	14 × 37	7 100	EOS
5	46	14.× 37	5 000	EOS
6	49	14 × 37	3 800	EOS
7-8	14	14 × 37	3 500	EOS
9	29, 70	14.5 × 52	^b 51 500	42 600
10	30, 23	14.5 × 52	^b 13 100	6 000
11	34, 72	14.5 × 59	^ъ 56 050	46 100
12	34, 22	14.5 × 59	^b 56 050	46 100
13-14	36	14.5 × 55	^b 52 300	43 200
15	37	14.5 × 60	41 900	34 100
16.	21, 75	14.5 × 52	^b 19 350	9 200
17	6, 2, 72	14.5 × 54	46 500	36 100
18	2, 73, 74	14.5 × 52	47 300	38 100
19	3, 4, 5	14.5 × 48.	35 000	26 400
20	52	14.5 × 52	43 400	36 600
21	71, 76	14.5 × 59	^b 56 050	46 100
22	71	14.5 × 59	^b 51 500	42 600

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(b) DOD - 1980

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Booster required
1-8	None			EOS
9	N-2B N-2A	14.5 × 55	^b 58 141	Tug
10	Three M-1	15 × 43	^b 16 399	Tug
11	Two S-4	.9 × 60	20 000	EOS
12	S-2B	15 × 60	30 574	Tug
13	C-1 C-3A	15 × 48	^ъ 50 980	Tug
14	Three N-2A	14.5 × 55	48 490	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(c)	NASA	- 1981
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Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
1	61	14 × 40	20 000	EOS
2-6	62	14 × 30	20 000	EOS
7	63	14 × 30	20 000	EOS
8	66	14 × 58	33 000	EOS
9	67	14 × 45	25 000	EOS
10-11	38	14 × 54	27 500	EOS
12-13	39	14 × 51	30 000 -	EOS
14	42	14 × 37	6 000	EOS
15-16	44, 14	14 × 50	9 200	EOS
17	47, 1	14 × 40	7 420	EOS
18	15	14 × 60	30 000	EOS
19	28	15 × 60	^b 38 400	23 600
20	29, 27, 72	14.5 × 58	^c 53 600	<u>ነ</u> ት 200
21	30, 23	14.5 × 52	^c 13 100	· 5 100
22-23	35	14.5 × 55	^c 51 400	42 500

^aBased on the minimum propellant required to place payloads in orbit.

bThe tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(c) NASA - 1981 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Round trip minimum tug propellant required
24	36	14.5 × 55	^b 52 300	43 200
25	21, 25, 75	14.5 × 58	^b 21 000	9 700
. 26	2, 73, 72	14.5 × 52	47 300	38 100
27	3, 4, 5	14.5 × 48	35 000	26 400
28	8, 9	14.5 × 60	^b 60 900	47 600
29	50	14.5 × 52	40 300	26 800
30	70, 72, 76	14.5 × 60	^b 55 500	45 300
31	71, 72, 74	14.5 × 60	^b 57 1 00	47 500
32	72, 72, 73	14.5 × 52	48 000	38 500
33	77	12.0 × 15	2 500	7 700
3 4	77 (plus tug)	14.5 × 55	^b 14 500	acc ounted for in flight 33

 $^{^{\}mathrm{a}}$ Based on the minimum propellant required to place payloads in orbit. $^{\mathrm{b}}$ OMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(c) DOD - 1981

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1-10	None			EOS
11	Three M-1	15 × 43	b ₁₆ 399	Tug
12	S-4	.9 × 60	10 000	EOS
13	S-2A	15 × .60	b 59 279	Tug
14	C-4 C-3B	15 × 60	^b 36 754	Tug
15	C-1	14.5 × 48	49 178	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(d) NASA - 1982

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^u	Round trip minimum tug propellant required
1	14, 1, 44	14 × 53	9 920	EOS
2	16, 1, 44	14 × 53	9 920	EOS
3	3, 4,	14.5 × 48	^b 25 500	16 500
4	5	14.5 × 46	p ³⁰ 000	22 500
5	13, 16	14 × 59	24 500	EOS
6	14	14 × 13	3 500	EOS
7	21, 75	14.5 × 52	^c 19 400	9 200
8	22, 27, 29	14.5 × 52	^c 53 600	44 200
9	23, 30, 32	14.5 × 58.5	^c 14 100	5 300
10	24, 71, 76	14.5 × 59	^c 59 800	48 900
11	27,72	14.5 × 52	^c 51 400	42 500
12-13	3 5	14.5 × 55	^c 51 400	42 500
14-16	38	14 × 54	27 500	EOS
17-19	39	14 × 51	30 000	EOS
20-21	42	14 × 37	6 000	EOS

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}rm C}{\rm OMS}$ must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
	(d)	NASA - 1982 - Cond	cluded	,
22	53	14.5 × 52	^b 50 300	46 600
23-24	55	14.5 × 55	36 100	^c 28 400
25	60 payload	10 × 35	24 000	accounted for in flight 26
26	60 tug	14.5 × 40	^b 52 300	45 500
27-32	63	14 × 30	20 000	EOS
3 3	71	14.5 × 52	^b 51 500	42 600

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

^CThe tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(d) DOD - 1982

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lba	Booster required
1-10	None			EOS
. 11	C-1 N-2B	14.5 × 55	53 818	Tug
12	C-3B	14.5 × 47	^b 28 968	Tug
13-14	S-2B	15 × 60	30 574	Tug
15	S-4	9 × 60	10 000	EOS
16-17	Two N-2A	14.5 × 55	40 666	Tug
18	D-1	14.5 × 60	25 000	Tug

^aBased on the minimum propellant required to place payloads in orbit.

 $^{^{\}rm b}$ ABES will have to be removed to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(e)	NASA -	1983
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Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
1	1, 36	14.5 × 55	3 020	EOS
2	1, 35	14.5 × 55	2 720	EOS
3	3, 4	i4.5 × 56	^c 53 600	44 600
4	5, 14	14.5 × 59	29 900	22 500
5	17 up 13 down	14 × 54 up 14 × 46 down	27 000 21 000	EOS
6	14	14 × 13	3 500	EOS _
7	16, 44	14 × 50	9 200	EOS
8	16, 45	14 × 50	10 600	EOS
9	21, 77	12 × 27	5 000	8 600
10	23, 30	14.5 × 52	^c 13 100	5 100
11	24, 70	14.5 × 52	^c 52 600	43 400
12	27, 70	14.5 × 52	^e 52 600	43 400
13	28	15 × 60	^b 38 400	23 600
14	29, 72	14.5 × 52	49 900	41 600
15	35	14.5 × 55	^c 51 400	42 500
16	36	14.5 × 55	^c 52 300	43 200
17-20	38	14 × 54	27 500	EOS
21-22	39	14 × 51	30 000	EOS
23-28	63	14 × 30	20 000	EOS

⁸Based on the minimum propellant required to place payloads in orbit.

bThe tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(e) NASA - 1983 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions; ft (D × L)	Total payload weight, lba	Round trip minimum tug propellant required
29	64 up 66 down	14 × 32 up 14 × 58 down	22 000 33 000	EOS
30	67, 68	14 × 38 up 14 × 45 down	19 000 25 000	EOS
31	71, 76	15 × 59	^b 56 050	46 100
32	72,73	14.5 × 52	45 600	37 100
33	75,77	12 × 21	3 500	10 100
34	77 tug	14.5 × 55	^b 17 900	accounted for in flight 9
35	77 tug	14.5 × 55	^b 19 500	accounted for in flight 33
36	74, 71	14.5 × 59	^b 55 200	45 600

^aBased on the minimum propellant required to place payloads in orbit.

 $^{^{}b} \text{OMS}$ must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(e) DOD - 1983

(-,				
Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Booster required
1-10	None			EOS
11	D-1	14.5 × 60	25 000 .	Tug
12	C-2 C-3A N-2B	15 × 59	^b 58 496	Tug
13	- C-2	14.5 × 52	51 418	Tug
14	Three N-2A	15 × 55	48 490	Tug
15	C-4 Two S-3	15 × 60	ė 39 852	Tug
16	S-2B	15 × 60	30 574	Tug
17	Two S-3	14.5 × 45	b13 009	Tug
18	S-4	9 × 60	10 000	EOS
19	Three M-1	14.5 × 45	^b 16 399	Tug
20	N-2A	14.5 × 55	22 280	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100-n. mi. circular orbit.

 $^{^{\}rm C}{\rm OMS}$ must be offloaded and the ABES removed to place this payload in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(f) NASA - 1984

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
1	1, 16	14 × 16		Too
			4 220	EOS .
2	2, 10	· 15 × 52	47 600	38 200
3	3, 4, 5	15 × 48	35 000	26 400
· 4	7, 30	14.5 × 52	^b 13 800	4 850
5	11	14.5 × 52	32 700	24 000
6	14	14 × 13	3 500	EOS
. 7	16 .	14 × 13	3 500	EOS
8	18	14 × 13	3 500	EOS
9	c18, 19 Centaur + another kick stage	14.5 × 43+	38 000+	EOS
10	.21, 75	14.5 × 52	19 350	9 200
11	22, 70	14.5 x 52	47 300	38 100
12	28	15 × 60	^d 38 400	23 600
13	29, 31	14.5 x 52	^b 49 750	41 500
14-15	35	14.5 × 55	^b 51 400	42 500
16	36	14.5 × 55	^b 52 300	43 200
17 .	37	14.5 × 60	49 000	41 200

^aBased on the minimum propellant required to place payloads in orbit.

 $^{^{\}rm b}{\rm OMS}$ must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}text{C}}$ The tug does not have the ΔV capability; therefore, a kick stage was used.

 $^{^{}m d}_{
m The}$ tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(f) NASA - 1984 / Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
18-21	38	14 × 54	27 500	EOS
22-24	39	14 × 51	30 000	EOS
. 25	40	14 × 54	29 500	EOS
26-27	41	14 × 41	22 500	EOS
28	61	14 × 40	20 000	EOS
29-34	63	14 × 30	20 000	EOS
35	71	14.5 × 59	^b 51 _, 500	42 600
36	71, 76	15 × 59	^b 56 050	46 100
37	14, 59	14 × 48 °	30 500	EOS

aOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

bABES will have to be removed to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(f) DOD - 1984

Shuttle flight no.	Payload designation	Total payload dimension, ft (D × L)	Total payload weight, lb ^a	Booster required
1-10	None ·			EOS
. 11	D-1	14.5 × 60	25 000	Tug
12	C-2 C-3A N-2B	15 × 59	^b 58 496	Tug
13	C-2	14.5 × 52	52 418	Tug
14-15	Two N-2A	14.5 × 55	40 666	Tug
16-17	S-2A	15 × 60	^b 59 279	Tug
18	S-4	9 × 60	10 000	EOS
19	Three M-1	15 × 43	^b 16 399	Tug

 $^{^{\}mathrm{a}}\mathrm{Based}$ on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued (g) NASA - 1985

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Round trip minimum tug propellant required
1	2,73	14.5 × 49	44 700	36 500
2	2,74	14.5 × 48	47 700	39 500
3 .	3, 4, 5	14.5 × 48	35 000	26 400
4	13, 18	14 × 59	24 500	EOS
5	14, 19	14 × 26	22 800	EOS
6	14, 60 tug	14.5 × 53	^ъ 55 800	^c 45 500
7	15 up	14 × 60	30 000	EOS
8	15 down	14 × 60	30 000	EOS
9	16	14 × 13	3 500	EOS
10	18, 60 payload	14 × 48	27 500	EOS
11	21, 77	12 × 27	5 000	8 600
12	23, 25, 30	14.5 × 58.5	c _{22 600}	13 600
13	29, 78, 78	14.5 × 58	^b 53 600	<u> </u>
14-15	35	14.5 × 55	^b 51 400	42 500
16-17	37	14.5 × 60	41 900	34 100
18-20	38	14 × 54	27 500	EOS
21-22	39	14 × 51	30 000	EOS

 $^{^{\}mathrm{a}}\mathrm{Based}$ on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

CABES will have to be removed to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(g) NASA ~ 1985 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
23-25	40	14 × 54	29 500	EOS
26-27	41	14 × 41	22 500	EOS
28	54 .	14.5 × 55	^ъ 60 300	46 200
29	57	14.5 × 55	^с 47 300	37 200
30	61	14 × 40	20 000	EOS
31-33	62	14 × 30	20 000	EOS
34-39	63	14 × 30	20 000	EOS
40	66	14 × 58	33 000	EOS
41	67, 68	14 × 45	25 000	EOS
42	70, 78, 78	14.5 × 58	^b 55 500	45 300
43	71	14.5 × 59	^b 51 500	42 600
. 44	71, 76	15 × 59	^ъ 56 050	46 100
45	75, 77	12 × 21	3 500	10 100
46	77 plus tug	14.5 × 55	^b 17 900	accounted for in flight 9
47	77 plus tug	14.5 55	^b 19 500	accounted for in flight 45

 $^{^{\}mathbf{a}}$ Based on the minimum propellant required to place payloads in orbit.

OMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}rm C}{\rm The}$ tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(g) DOD - 1985

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb a	Booster required
1-10	None			EOS
11	D-1 .	14.5 × 60	25 000	Tug
12	C-3A C-5	15 × 60	56 322	Tug
13	C-5	14.5 × 60	54 605	Tug
14-15	S-2B	15 × 60	30 574	Tug
16	Two S-3	12 × 45	^b 13 009	Tug
17-20	S-5	10 × 60	12 000	EOS

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(h) NASA - 1986

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight lb ^a	Round trip minimum tug propellant required
1-2	1, 16	14 × 16	4 200	EOS
3	3, 4, 30	14.5 × 56	^b 26 500	16 900
4	5	14.5 × 46	_p 30 000	22 500
5-6	14	14 × 13	3 500	EOS
7–8	18	14 × 13	3 500	EOS
9–10	20	14 × 13	3 500	EOS
11	21, 75	14.5 × 52	c 19 300	9 200
12 -	22, 29, 72	14.5 × 52	c ₅₃ 600	44 200
13	26 (2)	14.5 × 52	^c 12 7 00	7 700
14	28	15 × 60	^d 38 400	23 600
15-16	35	14.5 × 55	^e 51 400	42 500

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100 n. mi. circular orbit.

^COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

The tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(h) NASA - 1986 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant
17-19	39	14 × 51	30 000	EOS
20-23	40	14 × 54	29 500	EOS
24-25	41	14 × 41	22 500	EOS
26	58	14.5 × 55	b,c ₅₃ 600	43 100
27-29	61	14 × 40	20 000	EOS
30-37	63	14 × 30	20 000	EOS
38-39	71, 72	14.5 × 59	^ъ 56 050	46 100 ·
. 40	72, 76	14.5 × 52	^b 51 400	42 500
41	64 down	14 × 32	22 000	EOS

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

^CThe tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(h) DOD - 1986

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1-10	None			EOS
11	D-1	14.5 × 60	25 000	Tug
12.	C-2	10 × 52	51 418	Tug
. 13	Three N-2A	15 × 55	48 490	Tug
14	C-3B Two S-3	14.5 × 52	^b 29 270	Tug
15	S-2B	15 × 60	30 574	Tug
16	Three M-1	15 × 43	^c 16 399	Tug
17	N-2B N-2A	10 × 55	^c 58 141	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100-n. mi. circular orbit.

^COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(i) NASA - 1987

		(-) 10201 - 1901		
Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
1	1, 72, 73	11 × 52	46 400	37 100
2	16, 2	14.5 × 57	4 220	EOS
3	3, 4, 5	14.5 × 48	ъ,с _{57 900}	48 300
4	72, 8	14.5 × 52	48 400	40 100
5	57, 13 down	14.5 × 55 up 14 × 46 down	^c 47 400 27 000	37 200
6–7	14	14 × 13	3 500	EOS
8	16	14 × 13	3 500	EOS
. 9-10	18	14 × 13	3 500	EOS
11-12	20	14 × 13	3 500	EOS
13	23, 26 (2)	14.5 × 58.5	^b 20 800	8 400
14	30, 75, 21	14.5 × 58	^d 27 200	16 300
15	26 (2)	14.5 × 52	^b 12 700	7 700
16	27, 72 (2)	14.5 × 52	^b 54 100	44 300
17	74, 29	14.5 × 52	p [†] 8 †00	41 300
18–19	35	14.5 × 55	^b 51 400	42 500
20-21	36	14.5 × 55	^b 52 300	43 200

 $^{^{\}mathbf{a}}$ Based on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

^CThe tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

 $[\]ensuremath{^{d}}\xspace ABES$ will have to be removed to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(i) NASA - 1987 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Round trip minimum tug propellant required
22-26	40	14 × 54	29 500	EOS
27-28	41	14 × 41	22 500	,EOS
29-30	61	14 × 40	20 000	EOS
31-36	63	14 × 30	20 000	EOS
37	71, 72	14.5 × 59	^ъ 56 050	46 100
38	71, 76	15 × 59	^b 56 050	46 100

^aBased on the minimum propellant required to place payloads in orbit.

 $^{^{\}rm b}{\rm OMS}$ must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(i) DOD - 1987

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Booster required
1-10	None			EOS
11	D-1	15 × 60	25 000	Tug
12	C-3B	14.5 × 47	^b 28 968	Tug
13	C-5 N-2B	14.5 × 60	^e 59 972	Tug
14-15	S-2A	15 × 60	^c 59 279	Tug
16-17	S - 5	10 × 60	12 000	EOS
18	Three M-l	15 × 43	c _{16 399}	Tug
19-20	Two N-2A	14.5 × 55	40 666	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100-n. mi. circular orbit.

COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(j) NASA - 1988

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
1-2	16, 1	14 × 16	4 020	EOS
3	3, 4	14.5 × 48	25 500	16 500
4	72, 5	14.5 × 52	48 900	40 500
5	í2 (2)	14.5 × 50	^b 56 300	42 500
6-7	14	14 × 13	3 500	EOS
8	17 down	14 × 54	27 000	EOS
9	17 up	14 × 54	27 000	EOS
10	 18	14 × 13	3 500	EOS
11-12	20	14 × 13	3 500	EOS
. 13	30, 75, 21	14.5 × 58	^c 27 200	23 100
14	22, 29, 78	14.5 × 58	^b 53 600	44 200
15	27, 70, 78	14.5 × 58	^b 55 500	45 300
16	27, 71, 72	14.5 × 59	^b 59 800	48 900
17	28	15 × 60	^d 38 400	23 600
18-19	35	14.5 × 55	^b 51 400	42 500
20	36	14.5 × 55	^b 52 300	43 200
21-23	39	14 × 51	30 000	Eos
24-27	40	14 × 54	29 500	EOS
28-29	41	14 × 41	22 500	EOS
30	54	14.5 × 55	^b 60 300	46 200
31-38	63	14 × 30	20 000	EOS

 $^{^{\}mathbf{a}}_{\mathbf{B}}$ Based on the minimum propellant required to place payloads in orbit.

 $^{^{\}rm b}$ OMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}text{C}}\text{ABES}$ will have to be removed to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}rm d}_{\rm The}$ tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG
FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(j) NASA - 1988 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
39	64 up.	14 × 32	22 000	EOS
40	65 Part I up plus 65 part II up	14 × 59	^ъ 54 000	EOS
41	70, 78 (2)	14.5 × 58	^c 55 500	45 300
42	71, 76	14.5 × 59	^c 56 050	46 100

^aBased on the minimum propellant required to place payloads in orbit.

bABES will have to be removed to place this payload in a 100 n. mi. circular orbit.

COMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(j) DOD - 1988

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lba	Booster required
1-10	None	· .		EOS
. 11	D-1	15 × 60	25 000	Tug
· 12	C-2 C-3A N-2B	15 × 59	^b 58 496	Tug
13-14	S-2B	15 × 60	30 574	Tug
15	Two S-3	14.5 × 45	^b 13 009	Tug
16-17	Two N-2A	14.5 × 55	40 666	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR Δ V BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(k) NASA - 1989

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Round trip minimum tug propellant required
1-2	16, 1	14 × 16	· 4 220	EOS
3	3, 4, 5	14.5 × 48	35 000	26 400
4	11	14.5 × 52	32 700	24 000
5	10, 73	15 × 52	47 800	38 400
6	13 up	14 × 46	21 000	EOS
7-8	14	14 × 13	3 500	EOS
9-10	18	14 × 13	3 500	EOS
11-12	20 ,	14 × 13	3 500	EOS
13	21, 77	12 × 27	5 000	included in flight 43
14	23, 30, 32	14.5 × 58.5	^b 14 100	5 300 .
15	28	15 × 60	38 400	^c 23 600
· 16	29, 70	14.5 × 52	^b 51 500	42 600
17-18	35	14.5 × 55	^b 51 400	42 500
19	37, 72	14.5 × 60	^b 51 400	42 500
20	39	14 × 51	30 000	EOS
21-25	40	14 × 54	29 500	EOS
26-28	41	14 × 41	22 500	EOS
29	58	14.5 × 55	b,d ₅₃ 600	43 100
30-37	63	14 × 30	20 000	EOS
38	74, 71	15 × 59	^b 55 200	45 600
39	71, 76	15 × 59	^b 56 050	46 100
40	77, 75	12 × 21	^c 23 000	10 100

 $^{^{\}mbox{\scriptsize B}}\mbox{\sc Based}$ on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}text{C}}\text{ABES}$ will have to be removed to place this payload in a 100 n. mi. circular orbit.

dThe tug does not have the capability for a round trip and was therefore expended after the payload is placed in orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(k) NASA - 1989 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft	Total payload weight, lb ^a	Round trip minimum tug propellant
41	77	12 × 15	2 500	7 700
42	77 plus tug	14.5 × 55	^b 14 500	accounted for in flight 41
43	77 plus tug	14.5 × 55	^b 15 400	8 600
<u> </u>	77 plus tug	14.5 × 55	^b 17 000	10 100

a Based on the minimum propellant required to place payloads in orbit.

 $^{^{\}rm b}{\rm OMS}$ must be offloaded in order for the EOS to have capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(k) DOD - 1989

Shuttle flight no.	Payload designation	Total Payload dimensions, ft (D × L)	Total Payload weight, lb	Booster required
1-10	None			EOS
11	D-1	15 × 60	25 000	Tug
12	C-2 C-3A	14.5 × 59	^b 59 953	Tug
13	S-2B	15 × 60	30 574	Tug
14	Two S-3	14.5 × 45	^b 13 009	Tug
15-16	S-5	10 × 60	12 000	EOS
. 17	Three M-1	15 × 43	^b 16 399	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bollity to place this payload in a 100-n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(1) NASA - 1990

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Round trip minimum tug propellant required
1	2(2), 72	14.5 × 52	45 300	36 100
2	3, 4	14.5 × 48	^b 25 500	16 500
3	5	14.5 × 46	b _{29 200}	22 500
4	7; 30	14.5 × 52	e _{13 800}	4 850
5-6	d ₁₄ , 51 Centaur + another kick stage	14.5 × 53	37 000+	EOS
7	18, 51 payload	15 × 35.5	25 500	EOS
8	20, 51 payload	15 × 35.5	25 500	EOS
9-10	16	14 × 13	3 500	EOS
11	18	14 × 13	3 500	EOS
12	20	14 × 13	3 500	EOS
13	21, 25, 75	14.5 × 58	^b 21 000	9 700
14 .	22, 37	14.5 × 60	^b 51 400	42 500
15	29, 76	14.5 × 52	^b 49 900	41 600
16-17	35	14.5 × 55	^b 51 400	42 500
18	37	14.5 × 60	49 000	41 200
19-23	<u></u> 40	·14 × 54	29 500	EOS
24-27	41	14 × 41	22 500	EOS
28-35	63	14 × 30	20 000	EOS

 $^{^{\}mathbf{a}}\mathbf{B}\mathbf{a}\mathbf{s}\mathbf{e}\mathbf{d}$ on the minimum propellant required to place payloads in orbit.

 $^{^{\}rm b}{\rm OMS}$ must be offloaded in order for the EOS to have capability to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}text{C}} ABES$ will have to be removed to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}mbox{\scriptsize d}} \mbox{The tug does not have the ΔV capability; therefore, a kick stage was used.$

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Continued

(1) NASA - 1990 - Concluded

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lba	Round trip minimum tug propellant required
36	68 up 66 down	14 × 38 14 × 58	19 000 33 000	EOS
37	69 up 67 down	14 × 45 14 × 45	25 000 25 000	EOS
38	, 7 1	14.5 × 59	^b 51 500	42 600
39	71, 72	14.5 × 59	^b 56 050	46 100

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE V.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - TUG USED FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1979 - Concluded

(1) DOD - 1990

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lba	Booster required
1-10	None			EOS
11	D-1	15 × 60	25 000	Tug
12	C-2 C-3A N-2B	15 × 59	^b 58 496	Tug
13-14	S-2A	15 × 60	^b 59 279	Tug
15	Three M-1	15 × 43	^b 16 399	Tug
16-17	Two N-2A	14.5 × 55	40 666	Tug

^aBased on the minimum propellant required to place payloads in orbit.

bOMS must be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required	
(a) NASA - 1979					
1	43, 1	14 × 40	5 020	EOS	
2	48, 1	14 × 40	13 720	EOS	
3 .	13	14 × 46	21 000 .	EOS	
14	3, 4, 33	10 × 53	38 670	Centaur	
- 5	29, 31, 33	12 × 57	37 890	Centaur	
6	30, 21, 75	6.5 × 28	^b 18 920	Agena	

a In order to reduce the number of computer calculations, the total payload weight is based on maximum fuel loading of the booster.

(a) DOD - 1979

	Shuttle flight no.	Payload designation	Total payload dimensions, ft (D x L)	Total payload weight, lb ^a	Booster required
Ī	, l	None			EOS
	2	None			EOS

^aThe required fuel was calculated to determine the total payload weight.

bOMS will have to be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(b) NASA - 1980

		·		
Shuttle flight no.	Payload designation	Total payload dimensions, ft	Total payload weight, lb ^a	Booster required
1	42, 23	14 × 48.5	7 300	EOS, FW-4S
2-3	44	14 × 37	5 700	EOS
Ц	45	14 × 37	7 100	EOS
5	46	14 × 37	5 000	EOS
6	49	14 × 37	3 800	EOS
7–8	14	. 14 × 13	3 500	EOS
9	29, 36, 70	10 × 57	38 770	Centaur
10	30, 21, 75	6.5 × 40	18 920	Agena
11	34, 76	15 × 49	^b 37 615	Centaur
12 .	4, 34	10 × 57	37 615	Centaur
13	22 , 36	12 × 51	37 770	Centaur
14	74, 37	10 × 40	16 520	Agena
15	6, 2, 5	9 × 36	18 040	EOS, Agena
16	2, 71	15 × 49	.37 335	Centaur
17 ·	3, 72, 73	13 × 32	17 720	Agena
18	52	10 × 42	35 470	Centaur
19	71, 72	14 × 49	37 615	Centaur

^aIn order to reduce the number of computer calculations, the total payload weight is based on the maximum fuel loading of the booster.

bOMS will have to be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE VI. - EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(b) DOD - 1980

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight lb ^a	Booster required
1-10	None			EOS
11	N-2B Two N-2A	15 × 45	20 376	Centaur
12	Three M-1	. 15 × 23	4 797	Agena
13	S-2B	15 × 45	14 879	Agena
14	C-3A C-1 N-2A	15 × 52	24 178	Centaur
15	S-4	9 × 60	10 000	EOS

 $^{^{\}mathrm{a}}$ The required fuel was calculated to determine the total payload weight.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

Shuttle flight no.	Payload . designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required				
(c) NASA - 1981								
1	61	14 × 40	20 000	EOS				
2-6	62	14 × 30	20 000	EOS				
7	63 ·	14 × 30	20 000	EOS				
. 8	66 (up)	14 × 58	33 000	EOS				
9	67 (up)	14 × 45	25 000	EOS				
10-11	38	14 × 54	27 500	EOS				
12-13	39	14 × 51	30 000	EOS				
14	42 ·	14 × 37	6 000	EOS				
15	44, 1	14 × 40	6 420	EOS .				
16-17	14, 44	14 × 50	9 200	EOS				
18	15 (up)	14 × 60	30 000	EOS				
19	47	14 × 37	6 700	EOS				
20	28, 76	15 × 58	43 420	Centaur				
21	72(2), 29	10 × 60	37 070	Centaur				
· 22	30, 21, 23	12.5 × 38.5	18 520	Agena				
23	74, 72, 35	12 × 57	b,c _{38 170}	Centaur				
. 24	72, 27, 35	12 × 57	38 470	Centaur				
25	72, 70, 36	12 × 57	39 190	Centaur				
26	77(2), 25	12 × 55	8 100	3 FW-4S				
27	2, 9, 73	12 × 53	^b 41 890	Centaur				
28	3, 4, 5	14 × 28	17 620	Agena				
29	73, 8	9 × 28	15 820	Agena				
30	50	10 × 42	42 170	Centaur				
31	71, 72	14 × 49	37 615	Centaur				
32	77(2), 75	12 × 51	^b 8 100	3 FW-4S				

^aIn order to reduce the number of computer calculations, the total payload weight is based on maximum fuel loading of the booster.

OMS will have to be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

^cIf minimum propellant usage is assumed, then no OMS offloading would be required.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(c) DOD - 1981

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight,	Booster required
1-10	None			EOS
. 11	Three M-l	15 × 23	4 797	Agena
.12	S-4	9 × 60	. 10 .000	EOS
13-14	S-2A	15 × 55	26 073	Centaur
15	C-4 C-3B	15 × 40	11 675	Agena
16	C-1	9 × 28	10 162	Agena

^aThe required fuel was calculated to determine the total payload weight.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(d) NASA - 1982

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1	14, 1(2)	14 × 16	4 940	EOS
2	3, 4, 5	1.4 × 28.	b,c ₁₇ 620	Agena
. 3	13 (up)	14 × 46	21 000	EOS
14	14, 60 (booster)	14 × 43+	37 970+	EOS, Centaur + some other booster
5-6	16, 44	14 × 50	9 200	EOS
. 7	21, 75	11 × 17	^b 4 900	2 FW-4S
8	22, 24, 27	13 × 38	37 470	Centaur
9	42, 23	14 × 48.5	7 300	EOS, FW-4S
10	27, 35	12 × 51	37 470	Centaur
11	29, 72, 35	12 × 57	38 070	Centaur
12	42, 30, 32	13 × 54	8 820	EOS, 2 FW-4S
13-15	38	14 × 54	27 500	EOS
16-18	39	14 × 51	30 000	EOS
19	53	10 × 42	42 370	Centaur
20-21	55	10 × 45	. 35 370	Centaur
22	60 (payload)	10 × 35	24 000	Centaur
23-28	63	14 × 30	20 000	EOS
29	72, 71, 76	15 × 50	38 615	Centaur

⁸In order to reduce the number of computer calculations, the total payload weight is based on maximum fuel loading of the booster.

 $^{^{\}rm b}{\rm OMS}$ will have to be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

 $^{^{\}mathbf{c}}$ If minimum propellant usage is assumed then no OMS offloading would be required.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR ΔV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(d) DOD - 1982

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster
1-10	None			EOS
11	D-1	10 × 50	30 000	Centaur
12	N-2B Two N-2A	15 × 45	20 376	Centaur
13	C-1	14 × 45	18 681	Centaur
14	S-4	9 × 60	10 000	EOS
15-16	S-2B	15 × 45	14 879	Agena
17	C-3B	6 × 27	5 765	Agena

^aThe required fuel was calculated to determine the total payload weight.

TABLE VI. - EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(e) NASA - 1983

		<u>.</u>		
Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1-2	14, 1	14 × 16	4 940	EOS
3	3, 4, 5	14 × 38	37 270	Centaur
14	17 (up). 13 (down)	14 × 54 (up) 14 × 46 (down)	27 000 (up) 21 000 (down)	EOS
' .5	16, 44	14 × 50	9 200	EOS
6	16, 45	14 × 50	10 600	EOS
7.	21, 77(2)	12 × 57	^ъ 9 600	3 FW-4S
8	23, 30	10 × 17	2 600	2 FW-4S
9	24, 71	15 × 49	37 615	Centaur .
10	27, 28	15 × 56	43 420	Centaur
11	74, 70, 29	13 × 50	37 190	Centaur
12-13	35, 36	12 × 60	38 770	Centaur
14-17	38 ·	14 × 54	27 500	EOS
18-19	39	14 × 51	30 000	EOS
20~25	63 .	14 × 30	20 000	EOS
26	64 (up) 66 (down)	14 × 32 (up) 14 × 58 (down)	22 000 (up) 33 000 (down)	EOS
27	68 (up) 67 (down)	14 × 38 (up) 14 × 45 (down)	19 000 (up) 25 000 (down)	EOS
28	72, 73, 70	10.5 × 50	37 590	Centaur
29	72, 76, 71	15 × 60	38 615	Centaur
30	77(2), 75	12 × 51	^b 8 100	3 FW-4S

^aIn order to reduce the number of computer calculations, the total payload weight is based on maximum fuel loading of the booster.

bOMS will have to be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. circular orbit.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(e) DOD - 1983

				
Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1-10	None			EOS
• 11	· D-1	10 × 50	30 000	Centaur
12	N-2B Two N-2A	15 × 45	20 376	Centaur
13	C-2 Two N-2A	15 × 45	21 076	Centaur
14	C-3A C-2	10 × 39	15 851	Agena
15	S-2B	15 × 45	14 879	Agena
16	Three M-1	15 × 23	4 797	Agena
^b 17	C-4 Two S-3	15 × 50	4 900	Agena
18	S-4.	9 × 60	10 000	EOS
19	Two S-3	6 × 25	5 163	Agena

^aThe required fuel was calculated to determine the total payload weight.

bOMS will have to be offloaded in order for the EOS to have the capability to place this payload in a 100-n. mi. circular orbit.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS LOADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Continued

(f) NASA - 1984

Shuttle flight no.	Payload designation			Booster required	
1	16, 1	14 × 16	4 220	EOS	
2	2, 10, 11	15 × 54	38 990	Centaur	
3	3, 4, 5	14 × 28	17 620 ·	Agena	
. 4	7, 30	11.5 × 17	3 500	2 FW-4S	
5	14, 59 (payload)	14 × 48	30 500	EOS	
6	14, 71	14 × 52	20 465	EOS, Agena	
7	16, 35	14 × 48	20 320	EOS, Agena	
. 8	18, 22	14 × 39	19 320	EOS, Agena EOS, Agena	
9	18, 37	14 × 53	19 320		
10	21, 75	11 × 17	^b 4 900	2 FW-4S	
11	28 ·	15 × 50	42 420	Centaur	
12	70, 29, 31	13 × 54	37,310	Centaur	
13	35, 36	12 × 60	38, 770	Centaur	
14-17	38	14 × 54	27 500	EOS	
18–20	39	.14 × 51	30 000	EOS	
21	40	14 × 54	29 500	EOS	
22-23	41	14 × 41	22 500	EOS	
5 _j t	59 (booster)	10 × 30+	34 470+	EOS	
25 .	61	14 × 40	20 000	EOS	
26-31	63	14 × 30	20 000	EOS	
32	71, 76	15 × 49	37 615	Centaur	

^aIn order to reduce the number of computer calculations, the total payload weight is based on maximum fuel loading of the booster.

Since the tug becomes available in 1985, EOS flights for years 1985 through 1990 are the same as those defined in table V.

bOMS will have to be offloaded in order for the EOS to have the capability to place this payload in a 100 n. mi. ciruclar orbit.

TABLE VI.- EARTH ORBIT SHUTTLE TRAFFIC MODELS - KICK STAGES USED

FOR AV BEYOND EARTH ORBIT SHUTTLE CAPABILITY WITH PAYLOADS

LÖADED SIDE-BY-SIDE AND TUG AVAILABLE IN 1985 - Concluded

(f) DOD - 1984

Shuttle flight no.	Payload designation	Total payload dimensions, ft (D × L)	Total payload weight, lb ^a	Booster required
1-10	None			EOS
11	D-1	10 × 50	30 000	Centaur
12	N-2B Two N-2A	15 × 45	20 376	Centaur
13	Three M-1	15 × 23	4 797	Agena
14	S-14	9 × 60	10 000	EOS
15-16	S-2A	15 × 55	26 073	Centaur
17	C-3B C-2 N-2A	10 × 57	27 387	Centaur
18	N-2A C-2	15 × 45	24 962	Centaur

^aThe required fuel was calculated to determine the total payload weight.

Since the tug becomes available in 1985, EOS flights for years 1985 through 1990 are the same as those defined in table V.

TABLE VII.- EOS FLIGHTS ASSOCIATED WITH TWO TUG AVAILABILITY TIMES, 1979 AND 1985

														_	
Totel	9	ν. ΑΤ φ	574		399	580	,00		196		253		ם כ	733	253
1990	Ç	ξ	52		39	22	7.		17		23		ţ	-	ຊ
1989	. :	1	54		77	4	,		17		ส		ţ	7	្ដ
1988	2	# Y	85		715	. 65	?		17		22			-	52
1987	٩	9	55	-	38	55	,,		50		25		ć	Q V	25
1986		Ţ †	25		. [4		·		17	,	77.		,	- -	7₹
1985	ţ	_ †	62		1 47	69	;		20		22		ç	3	22
1984	100	ō	74		35	747			19		25		α	2	25
1983	70	2	25		30	55	(20		59		0.	, T	53
1982		ว	45		53	917			18		ส		17	ī	ผ
1981	i	ţ,	52		32	7,7			15	,	87 		76	2	18
1980	8	7	3 ,		19	#			77		22			`	22
₁₉₇₉	v	•	11		9	14			αı		α		٥	ı	α
81978										•					
Mode	NASA			NASA	flights	NASA payloads		god	₽		payloads	Ş	flights	200	payloads
Description	Tug available in 1979 -	placed	side-by-side	Tug available	payloads	placed side-by-side		Tug available	payloads	placed	side-by-side	Tug available	n 1965 -	placed	side-by-side

⁹Three dedicated NASA and one dedicated DOD flights for the year 1978 will be defined by NASA Headquarters and are not included in this table.

^bFour dedicated NASA and two dedicated DOD flights for the year 1979 will be defined by NASA Headquarters and are not included in this table.

TABLE VIII. - NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS BY INCLINATION

(a) NASA - tug available in 1979 and payloads stacked side-by-side

		I	nclinati	.on			
Year	28.5	30	55	65.	75	^a 90	Total
1979	5	1					6
1980	17	3				3	23
1981	12	ъ ₃	12	2		5	34
1982	7	^b 8	9	3		6	33
1983	14 .	с 3	12	2	!	-5	36
1984	13	e ₅	12	3	2	2	37
1985	13	6	19	2	2	5	47
1986 .	9	7	16	3	2	4	41
1987	13	7	13		2	3	38
1988	13	.9	14	3	2	1	42
1989	10 .	a ₉	14	1	3	7	դ դ
1990	10	6	15		4	Т	39
Total	135	67	136	19	17	45	420
Percent	32.2	16.0	32.4	4.6	4.1	10.7	100.0

^aFor sun synchronous orbits, the EOS carries the tug plus payload to a 100-n. mi. circular orbit at an inclination of 90° and the tug is used to make the plane change.

bTwo flights contain a 30° payload combined with a 28.5° payload.

One flight contains a 30° payload combined with a 28.5° payload.

done flight contains a 30° payload combined with a 29° payload.

TABLE VIII.- NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS BY INCLINATION - Continued

(a) DOD - tug available in 1979 and payloads stacked side-by-side

Year	28.5	30 .	63.4	90 ^b	^a Total
1979					
1980	1	2	1	2	6
1981	2		1	2	5
1982	1	2	2	2	7
1983	2	2	1	14	9
1984	14	2		2	8
1985	2		2	5	9
1986	ı	2	ı	2	6
1987	3	2		14	9
1988	.1	. 2	2	1	6
1989	1		1	. 4	6
1990	3	2		1	6
Total	21	16	11	29	71
Percent	27.3	20.8	14.3	37.6	100

^aMissions D-1, SESP, and support were not included in the total because their orbital parameters were not available.

 $^{^{\}rm b}$ Payloads with inclinations greater than 90 $^{\rm o}$ were offloaded at 90 $^{\rm o}$ with the delivery vehicle making the plane change.

TABLE VIII .- NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS

BY INCLINATION - Continued

(b) NASA - tug available in 1985 and payload stacked side-by-side

		Inclination ·								
Year	28.5	30	55	65	75	90	Sun synchronous	Total		
1979	4	1				a _l		6		
1980	14	3			<u> </u>	a ₂		19		
1981	11	ъ3	12	2	[c ₂	2	32		
1982	6	7	9	3		3	1	29		
1983	10	3	12	2		1	2	30		
1984	7	d,e ₆	12	3	2	1	1	32		
1985	13	6	19	2	2	5		47		
1986	9	7	16	3	2	14		41		
1987	13	7	13		. 2	3		38		
1988	13	9	14	3	2	1		42		
1989	10	f ₉	14	1	3	7		71,7		
1990	10	6	15	···	<u>,</u> †	· 14		39		
Total	120	67	136	19	17	34	6	399		
Percent	30.1	16.8	34.1	4.7	4.3	8.5	1.5	100.0		

^aOne flight contains two sun synchronous payloads.

One flight contains a 30° payload combined with a 28.5° payload.

^cOne flight contains a sun synchronous payload.

done flight contains a 30° payload combined with two 28.5° payloads.

 $^{^{\}rm e}$ Three flights contain a 30° payload combined with a 28.5° payload and one flight with a 30° payload combined with two 28.5° payloads.

fone flight contains a 30° payload combined with a 29° payload.

TABLE VIII.- NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS

BY INCLINATION - Concluded

(b) DOD - tug available in 1985 and payload stacked side-by-side

	Inclination				·
Year	28.5	. 30 .	63.4	9 <u>0</u> b	a Total
1979				,	
1980		2	1	2	5
1981	3		1	2	6
1982		2	2	2	6
1983	1	2	1	14	8
1984	2	3		2	7
1985	2		2	5	9
1986	1	2	1	. 2	6
1987	. 3	2		4	9
1988	1	. 2	2	1	6
1989	1		1	<u>†</u>	6
1990	3	2		1	6
Total	17	17	11	29	74
Percent	23.0	23.0	14.9	39.1	100

^aMissions D-1, SESP, and support were not included in the total because their orbital parameters were not available.

 $^{^{}b}\textsc{Payloads}$ with inclinations greater than 90° were offloaded at 90° with the delivery vehicle making the plane change.

TABLE IX. - TOTAL PAYLOAD TO ORBIT (LB)

(a) - NASA tug available in 1979 and payloads stacked side-by-side

			Inc	Inclination			
Year	28.5	30	55	65	75	06 ₈	Total
1979	107 190	21 000				22 700	150 890
1980	573 750	50 400		•		38 450	662 600
1981	564 720	147 300	288 000	000 09		57 100	1 017 120
1985	338 940	226 800	202 500	000 06		95 000	953 240
1983	259 690	55 000	329 000	000 09		29 000	1 062 690
1984	546 320	99 300	279 500	000 06	145 000	33 150	1 093 270
1985	559 150	238 200	000 †9†	000 09	000 St	68 500	1 434 850
1986	366 740	74 600	360 000	000 06	η2 000	88 500	1 024 840
1987	583 420	95 400	347 500		1,5 000	002 09	1 132 020
1988	556 390	188 100	354 000	000 06	145 000	27 200	1 260 690
1989	396 490	143 400	342 500	30 000	67 500	91 500	1 071 390
1990	412 950	95 000	341 500		90 000	90 200	1 029 650
Total	5 565 750	1 334 500	3 308 500	570 000	382 500	732 000	11 893 250

a Sun synchronous payloads plus tugs were offloaded at an inclination of 90° and the tug performed the plane change.

TABLE IX.- TOTAL PAYLOAD TO ORBIT (LB) - Continued

(a) - DOD tug available in 1979 and payloads loaded side-by-side

		Incl	ination		
Year	28.5	30	63.4	^a 90	Total
1979					
1980	50 980	99 831	30 574	36 390	217 775
1981	108 457		35 754	26 399	170 610
1982	47 018	67 732	61 148	38 968	214 866
1983	96 314	57 170	30 574	72 460	256 518
1984	214 872	33 866		26 399	275 137
1985	97 327		61 148	87 103	245 578
1986	44 618	93 031	30 574	45 669	213 892
1987	171 730	67 732	·	69 357	308 819
1988	51 696	67 732	61 148	13 099	193 675
1989	53 153		30 574	53 498	137 225
1990	170 254	67 732		16 399	254 385
Total	1 106 419	554 826	341 494	485 741	2 488 480

 $^{^{}a}$ Payloads having inclinations greater than 90° are offloaded at 90° with the plane change being made by the delivery vehicle.

The payload site for the D-1, SESP, and support missions are not included because the necessary information was not available.

TABLE IX.- TOTAL PAYLOAD TO ORBIT (LB) - Continued

(b) - NASA tug available in 1985 and payloads stacked side-by-side

			Ι	Inclination				
Year	28.5	98	. 55	59	75	⁸ 90	Sun synchronous	Total
1979	95 300	21 000					18 920	135 220
1980	306 300	016 01				7 300	18 920	373 490
1981	345 965	149 170	270 620	000 09		24 520	16 200	166 675
1982	170 025	201 020	202 500	000 06		33 740	006 7	702 185
1983	322 720	55 000	329 000	000 09		2 600	.17 700	787 020
1984	228 870	75 470	279 500	000 06	η5 000	3 500	006 7	787 240
1985	266 550	234 650	513 395	000 09	145 000	85 490	- 1	1 505 085
1986	161 180	74 585	360 000	000 06	145.000	106 380		1 167 145
1987	710 005	89 270	347 500		145 000	71 360		1 263 135
1988	691 780	223 440	354 000	000 06	η5 000	37 670		1 441 890
1989	1,86 550	143 355	362 910	30 000	005 19	95 610		1 185 925
1990	493 585	141 000	341 500		90 000	103 360	·	1 169 445
Total	4 968 830	1 348 930	3 360 925	570 000	382 500	571 530	81 540	11 284 455

 $^{
m a}_{
m From}$ 1985 on sun synchronous payloads plus tugs were offloaded at an inclination of $90^{
m o}$ and the tug performed the plane change.

TABLE IX. - TOTAL PAYLOAD TO ORBIT (LB) - Concluded

(b) - DOD tug available in 1985 and payloads loaded side-by-side

		Inc	lination		
Year	28.5	30	63.4	^a 90	Total
1979					
1980		58 190	14 879	14 797	87 866
1981	62 308		11 675	14 797	88 780
1982	-	52,693	14 879	15 765	83 337
1983	17 159	55 088	14 879	35 552	122 678
1984	52 146	79 543		14 797	146 486
1985	97 327		61 148	87 103	245 578
1986	44 618	93 031	30 574	45 669	213 892
1987	171 730	67 732		69 357	308 819
1988	51 696	67 732	61 148	13 099	193 675
1989	53 153		30 574	53 498	137 225
1990	170 254	67 732		16 399	254 385
Total	720 391	541 741	239 756	380 833	1 882 721

 $^{^{}a}$ Payloads having inclinations greater than 90° are offloaded at 90° with the plane change being made by the delivery vehicle.

The payload site for the D-1, SESP, and support missions are not included because the necessary information was not available.

TABLE X.- ENERGY STAGES REQUIRED

	(B) N	ASA - ti	ng avai	able ir	1979	and pay	oads lo	aded si	NASA - tug available in 1979 and payloads loaded side-by-side	ide			
	1979	1980 1981	1961	1982	1983		1984 1985	1986	1987	1988	1989	1990	Total
Tug flights Tugs expended Centaurs expended Agenas expended FW-4S expended Number of orbital assemblies	m00000	1.4 1.0 0 0	15 1 0 0 0	₹0000 r	4.0000	14 00 0 1	11.7 00 00 E.	0000 0000	115 00 00 00	14 1 0 0 0	0000m	21 0 0 0 0 0 0 0	160 14 2 0 0 13

^aFull usage is not made of tugs because they are required to be expended before nominal end of lifetime. Centaur plus another kick stage.

in 1979 and payloads loaded side-by-side

	(B)	000 - tu	g avaı	(a) DOD - tug available in 19/9 and payloads loaded since of since	19.79.B	nd pay	or spec	Te name	10-01	}			
	1979	1980	1981	1982	1983	1981	1985	1986	1987	1988	1989	1990	1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 Total
Tug flights Tugs expended Centaurs expended Agenas expended FW-LS expended Number of orbital assemblies		ľ.	дH	7	91	1	9	Ft	8 1	-	2	FH	73

TABLE X.- ENERGY STAGES REQUIRED - Concluded

	(b) NASA - tug available in 1985 and payloads loaded side-by-side	20				-			,				
-	1979	1980	1981	1982	1983	1984	1984 1985	1986 1987	1987	1988	1989	1990	Total
Tug flights Tugs expended Centaurs expended Agenas expended FW-4S expended Number of orbital assemblies	002400	001410	008890	000141	000000	0012101	1,7 8,3 0 0 0 3	0000 0000	24 00 00 00	41 0000	64. 60. 00. 00. 00.	12 0 0 0 0	86 10 13 13 10

^aFull usage is not made of tugs because they are required to be expended before nominal end of lifetime.

^bCentaur plus another kick stage.

 $^{\mathsf{c}}$ One flight requires Centaur plus another kick stage.

(b) DOD - tug available in 1985 and payloads loaded side-by-side

	1979	1980	1981	1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990	1983	1984	1985	1986	1987	1988	1989	1990	Total
Tug flights Tug expended Centaurs expended Agena expended FW-4S expended Number of orbital assemblies		ma	01 M	mm	w rv	1	٥	·	8 -1	7	1	FI	40 17 14 14

Energy stages for the D-1, SESP, and support missions are not included because the necessary orbital parameters were not available.

TABLE XI.- NUMBER OF EARTH ORBIT SHUTTLE FLIGHTS PER YEAR

ancludes the first 10 flights to be defined by NASA Headquarters.

TABLE XII.- NUMBER OF FLIGHTS REQUIRING OFFLOADING OF OMS OR REMOVAL OF ABES

(a) NASA - tug available in 1979 and payloads loaded side-by-side

	_	_													-
		Both													
	Total	ABES	-	-		2			,	N	н	N		2	12
		OMS	7	٥	10	10	10	-	10	6	7	10	11	ω	106
		Both													
	96 _n	ABES				8			ч	N	н		-	N	п
		OMS		Ω.	m	C)	m	н	N	N	CV		. ⊐	N	23
		Both.									·-				
	75	ABES					-								
ation		OMS							-						
Inclination		Both													
	65	ABES													
		OMS													
		Both													
	55	ABES										٦			1
		OMS		<u>, , , , , , , , , , , , , , , , , , , </u>											
		Both													
	8	ABES													
		OMS				N			C)	7		N	н		8
		Both													
	28.5	ABES													
		OMS	τ		-	9	7	v	9	9	6	ھ	9	9	75
_		Year	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	Total

⁸Sun synchronous payloads plus tugs were off-loaded at an inclination of 90° and the tug performed the plane change.

TABLE XII.- NUMBER OF FLIGHTS REQUIRING OFFLOADING OF OMS OR REMOVAL OF ABES - Continued

(a) DOD - tug available in 1979 and payloads loaded side-by-side

Year OMS ABES Both OMS ABES ABES ABES ABES ABES ABES ABES ABES </th <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>Incl</th> <th>Inclination</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th>								Incl	Inclination							
OMS ABES Both OMS ABES	;		28.5			30			63.4			96 ₈			Total	
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Year	SMO	ABES	Both	OMS	ABES	Both	OMS	ABES	Both	OMS	ABES	Both	OMS	ABES	Both
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1 3 3 11 2 11 2	1987	Н									т	ч		4	ਂ ਜ	· .
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TABLE XII. - NUMBER OF FLICHTS REQUIRING OFFLOADING OF ONS OR REMOVAL OF ABES - Continued (b) MASA - tug available in 1985 and payloads loaded side-by-side

	ĺ											Inclination	tion											
Year		28.5			30			55			65			75	-		8		I A	Sun	s a	£	Total	
	OMS	ABES	Both	OHS	ABES	Both	OMS	ABES	Both	OMS	ABES	Both	OMS	ABES	Both	OMS	100	Both	OMS	ABES	Both	OMS	10	Both
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1989	9			7												-						3	٠-	
1990	9								•							=	—					ส	-	
	: '			,												α	C)					6 0	~	
Total	1			٥												ā	8					9	α	
в Т	f mini	od mum:	alf minimum booster fuel usage were assumed, no OMS offloading would be required	uel usa	ige were	assum(ed, no	OMS off	loading	Vould	he rea	ntred											,	Ì

TABLE XII. - NUMBER OF FLIGHTS REQUIRING OFFLOADING OF OMS OR REMOVAL OF ABES - Concluded

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By Both	CI .
Sug available in 1985 and payloads loade Inclination 30 63.4 ABES Both OMS ABES Both OMS 1 1 1 2 1 1 1 1 1 1 1 1	_
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30 63.4 ABES Both OMS ABES	
30 ABES Both OMS	
30 ABES Both	,
30 ABES	
OMS OMS	
(b) 1 Both	ŧ
28.3 ABES	
OMS 1 1 3 3	5
Year 1979 1980 1982 1983 1985 1986 1986 1986	Total

Payloads with inclinations greater than 90° were offloaded at 90° and placement completed by the appropriate vehicle.

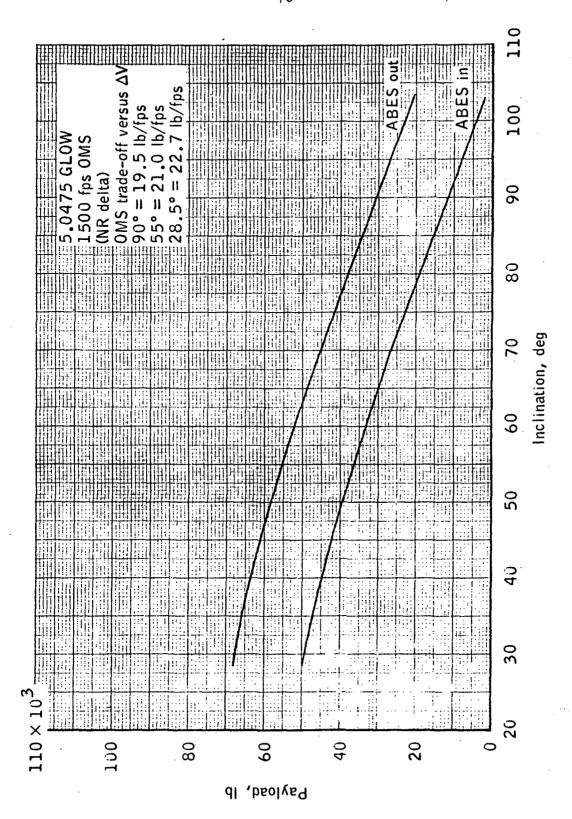


Figure 1.- Earth orbit shuttle payload capability versus inclination.

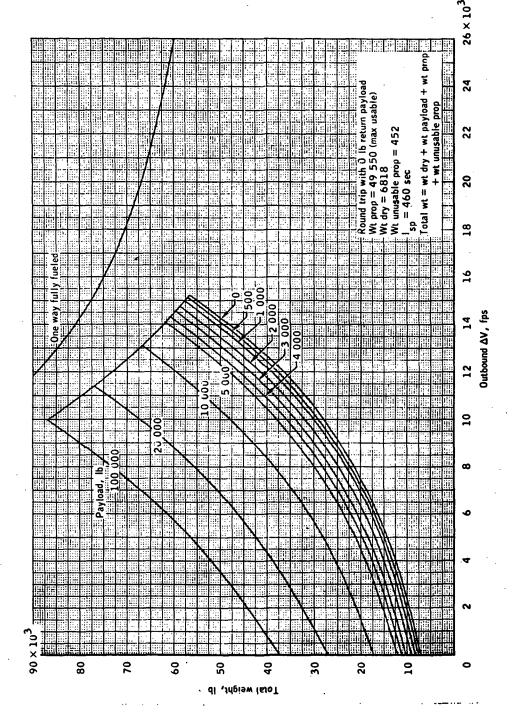


Figure 2. - Tug capability curves.

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